



Rheological Behavior in Decollement Folding: Appalachian Plateau

R. C. Fletcher

Department of Geosciences, Pennsylvania State University, U.S.A. (rfletche@geosc.psu.edu)

In a pioneering study Sherwin (1972, ms) modeled decollement folding for sub-regions of the Appalachian Plateau, one centered on the Fir Tree Point Anticline, NY. Here, mean fold span \approx dominant wavelength $L_d \approx 11.2$ km, and stiff layer thickness $H \approx 2.2 - 2.4$ km, yield $L_d/H \approx 4.6$ to 5.2 . Decollement occurs within a weak layer with thickness $H_1 \approx 0.8$ to 0.5 km, or $T = H_1/H = 0.4$ to 0.2 . A satisfactory 3-layer isotropic viscous model satisfied criteria: (i) mechanical layers consistent with lithology in stratigraphic section; (ii) high deformation within observed interval, with negligible structural relief below; (iii) proper L_d/H ; and (iv) viscosity ratio $1/R = \eta_1/\eta_0$ not too large (≤ 150). Models satisfying (i) – (iv) were found for viscous layers, with neglect of gravity, but yielded maximum relative rates of amplification $q_d \approx 5$; for observed 10% layer-parallel shortening, amplification of $10 - 100$ requires $q_d = 23 - 46$. (ii) implies a 2-layer model is adequate; for this, with power-law stiff layer (stress exponent n), Schmalholz et al. (2002) verified that gravity could be neglected for such decollement folding and likewise felt modest values of q_d were acceptable. They obtained approximations: $L_d/H \cong \pi\theta^{-(1/6)}$, $\theta = n(\eta_1/\bar{\eta}) / (H_1/H)^3$, $q_d [2\pi(H/L_d)]^2 \cong 2n$. A fit for larger q_d requires $n \approx 10$ and $1/R \approx 1000$. Replacement of the welded base by a weak surface permits reduction in $1/R$ by a factor of 4; if, alternatively, the weak layer is anisotropic, the above results for a welded interface remain valid if η_1 is identified with the viscosity in layer-parallel shear, η_S . Arguing from an estimate of layer-parallel shear to shortening viscosity ≈ 0.03 (Chapple & Spang, 1974) allows a reduction in $1/R$ by a factor of 6. Other issues in estimation of rheological behavior and its uniqueness will be discussed based chiefly on this example.