



## **Fluid inclusion hydrogen and oxygen isotope analyses using the “Amsterdam Device”: a progress report**

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The Amsterdam Device is a continuous-flow preparation device for on-line  $\delta^2\text{H}$  and  $\delta^{18}\text{O}$  analysis of fluid inclusions in speleothem carbonate. The design is based on a relatively low-cost adaptation to a Thermo Finnigan TC-EA pyrolysis furnace. Standard specifications of the Thermo Finnigan TC-EA allow for simultaneous  $\delta^2\text{H}$  and  $\delta^{18}\text{O}$  analysis of 0.2 microliter of water, reproducible within 2 permil for  $\delta^2\text{H}$  and 0.5 permil for  $\delta^{18}\text{O}$  (1SD). The technical description of the Amsterdam device was published in 2006, together with the results of some first crushing experiments. These experiments showed that the technique works well for  $\delta^2\text{H}$  analyses, but not enough experiments were done at the time to evaluate the applicability of the device for  $\delta^{18}\text{O}$  analyses of the same samples.

Over the last year we have run extensive experiments with the so-called jump routine, which allows combined  $\delta^2\text{H}$  and  $\delta^{18}\text{O}$  analysis of the water released from a single crush. The jump routine is a standard feature in the software for our Thermofinnigan TC-EA and Delta XP, and involves a calibrated rapid magnet jump of the mass spectrometer in the time between the entry of the GC-separated  $\text{H}_2$  and  $\text{CO}$  peaks.

In these recent experiments we have made two main changes compared to the Vonhof et al (2006) protocol:

- 1: We have installed a reverse-flow carrier gas setup, which has decreased the memory effect on TC-EA analyses (Gehre et al., 2004). To accommodate that, we split the incoming carrier gas in two flows: A) a  $\sim 10$  ml/min flow entering at the bottom connector of the TCEA reactor, and B) a  $\sim 100$  ml/min carrier flow that leads through the crusher and cold trap to enter in the top of the glassy carbon reactor.

2: For the freezing protocol we apply an ethanol slush at  $\sim -90$  degrees Celsius, instead of liquid nitrogen applied in the older experiments. This is essential because isotopically distinct  $\text{CO}_2$  released from the crushed  $\text{CaCO}_3$  sample is trapped along with the inclusion water under liquid nitrogen temperature and contributes to the  $\delta^{18}\text{O}$  value analysed with the pyrolysis method. At ethanol slush temperatures, water will be trapped quantitatively and  $\text{CO}_2$  will not, leading to a inclusion water  $\delta^{18}\text{O}$  analysis unaffected by  $\text{CO}_2$  derived oxygen.

With this new protocol we have analysed speleothem material from different settings and a selection of results is presented. Often,  $\delta^2\text{H}$  and  $\delta^{18}\text{O}$  data plot near the Global Meteoric Water Line (GMWL), which lends support to the accuracy of the analyses. If data plot away from the GMWL it is usually the  $\delta^{18}\text{O}$  data that are off-set. These  $\delta^{18}\text{O}$  off-sets are believed to be analytical artefacts. Our experiments did not provide evidence for oxygen exchange between fluid-inclusion water and surrounding carbonate.

*References:*

Gehre, M., H. Geilmann, J. Richter, R. A. Werner, and W. A. Brand, 2004, Continuous flow  $^2\text{H}/^1\text{H}$  and  $^{18}\text{O}/^{16}\text{O}$  analysis of water samples with dual inlet precision: Rapid Communications in Mass Spectrometry, v.18, p. 2650–2660

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